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# INTERFACE CHARACTERISTICS OF ALUMINUM-COPPER OBTAINED BY EXPLOSIVE WELDING

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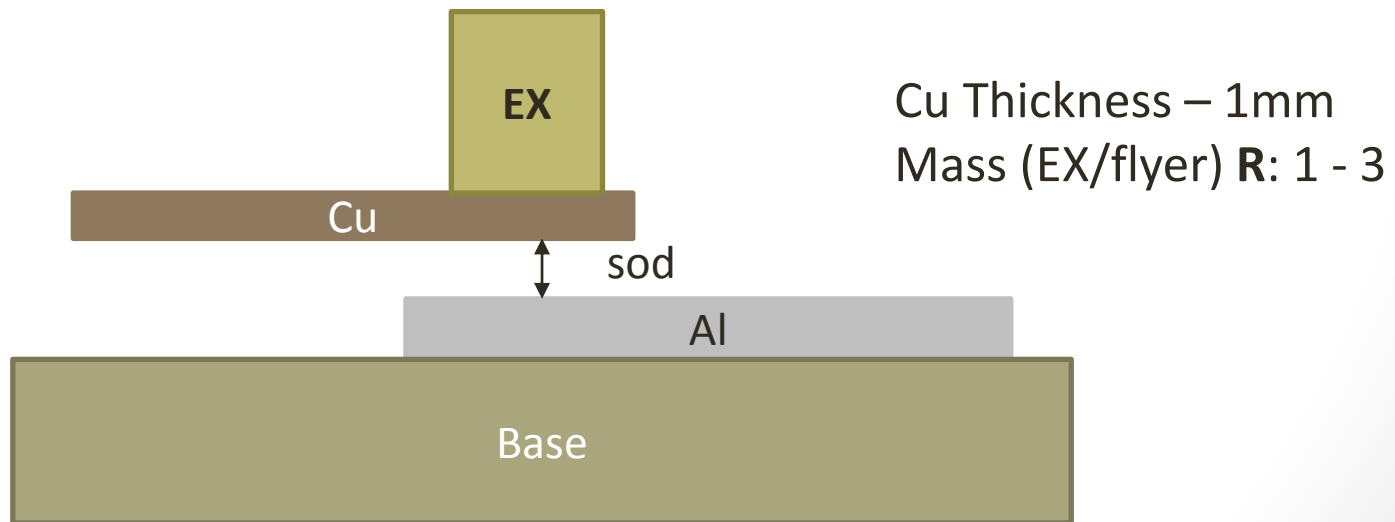


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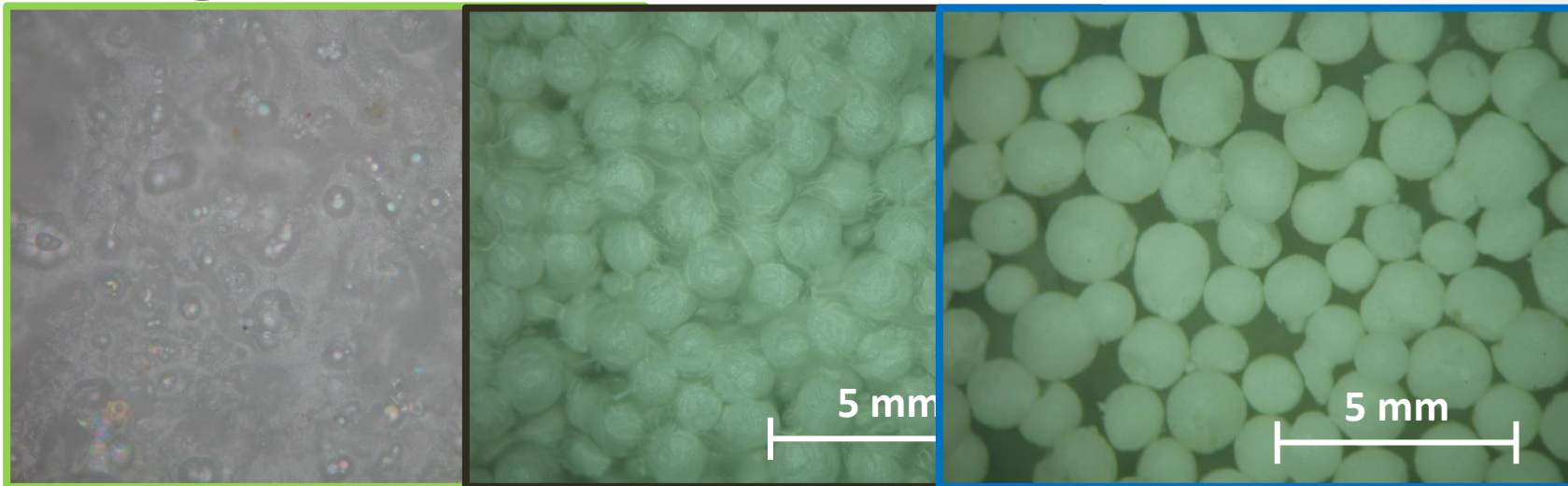
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# Objective

1. Preparation of Cu/Al full lap joint by explosive welding.
2. Study of the explosive nature and explosive/flyer mass ratio on the characteristics of the bonding interface.



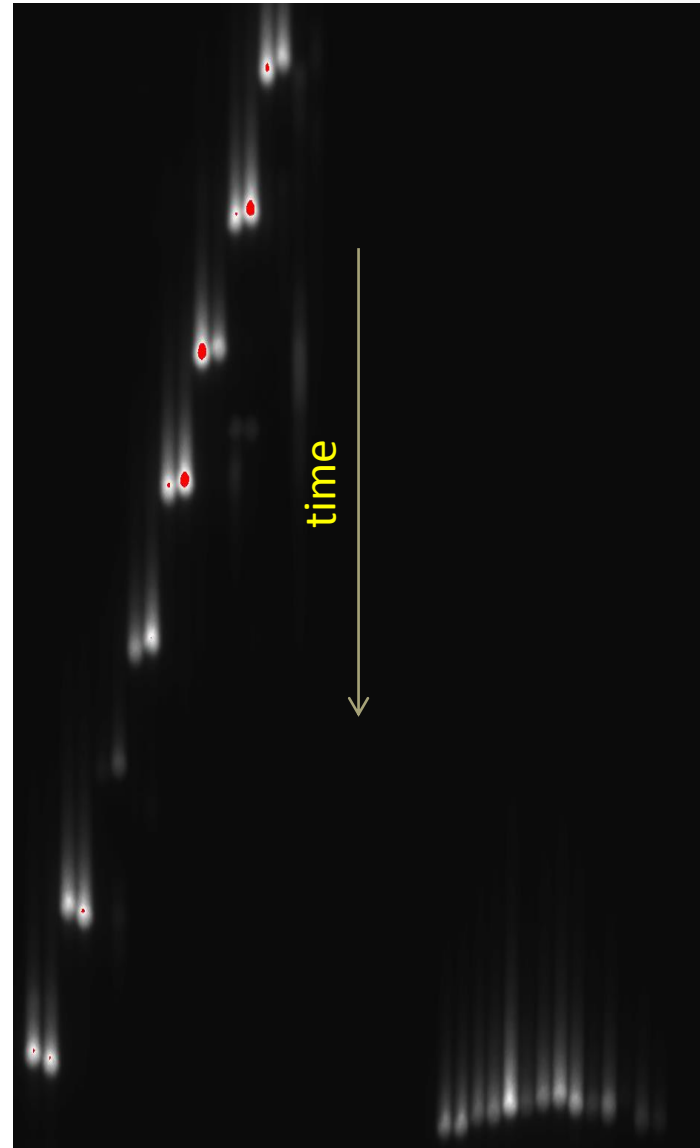
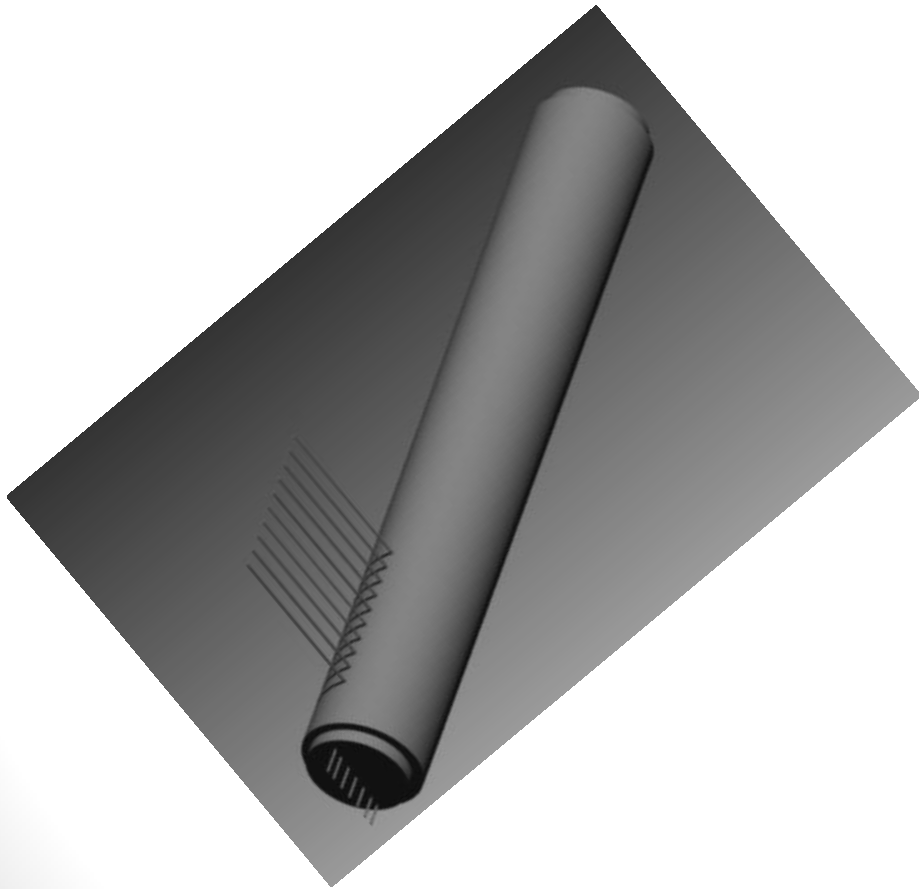
# Energetic Material



Emulsion Matrix	EPS (%)	HGMB (%)	ANFO (%)	$\rho_0$ (g/cm <sup>3</sup> )
85	-	15	-	0.76
98	1.2	-	-	0.90
20	-	-	80	0.82
-	-	-	100	0.80

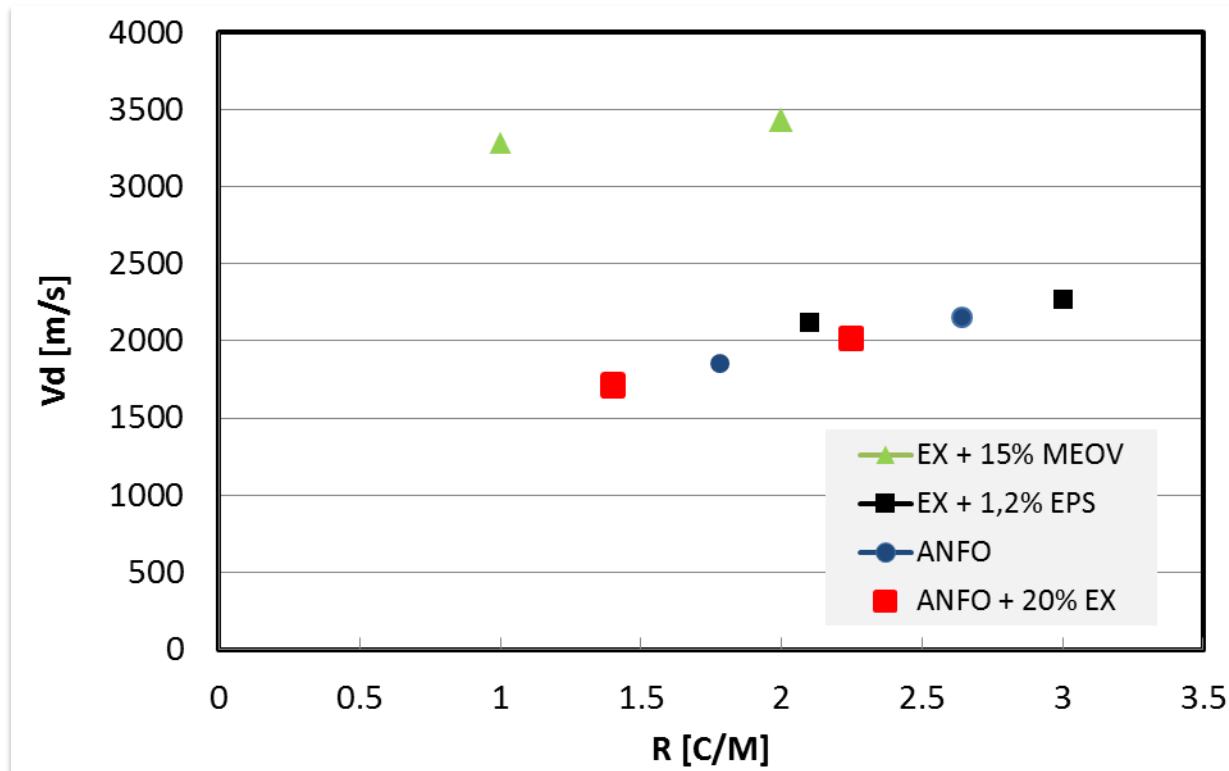


# Long charge teste- Detonation velocity



# Detonation velocity

Detonation velocity vs Explosive/flyer mass ratio (R)

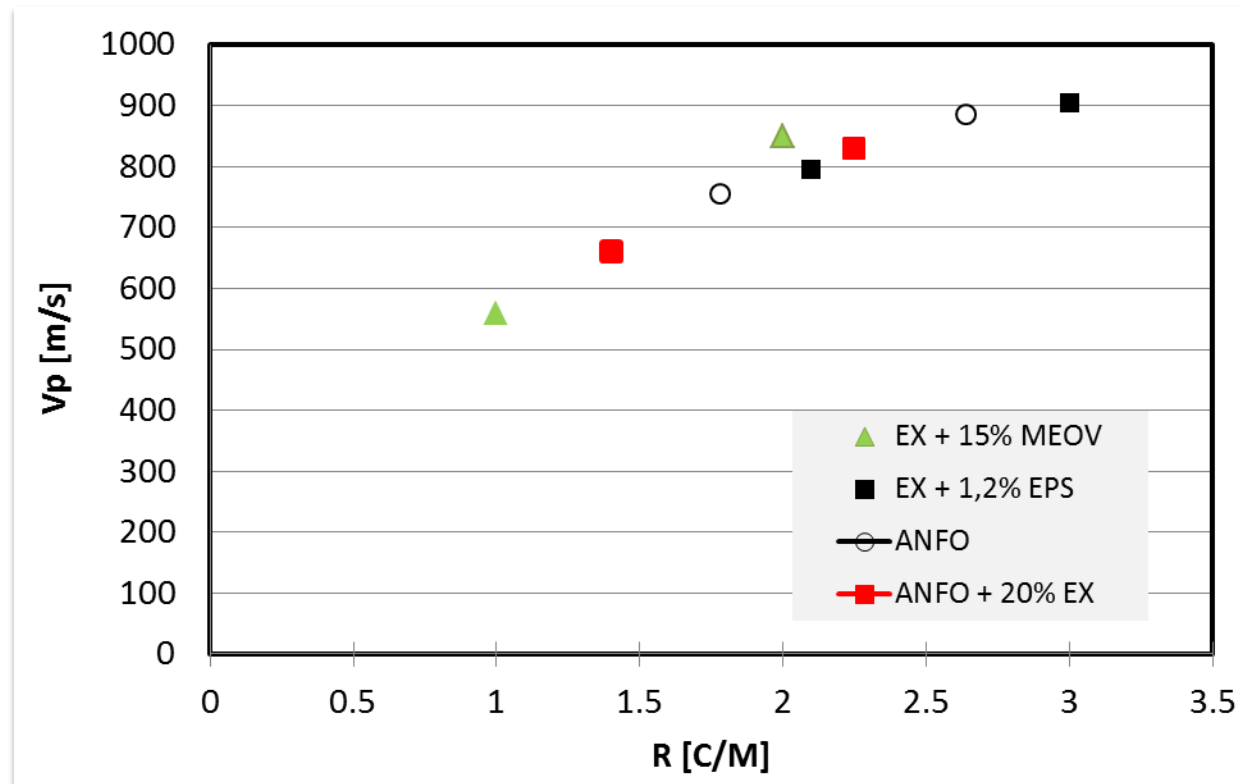


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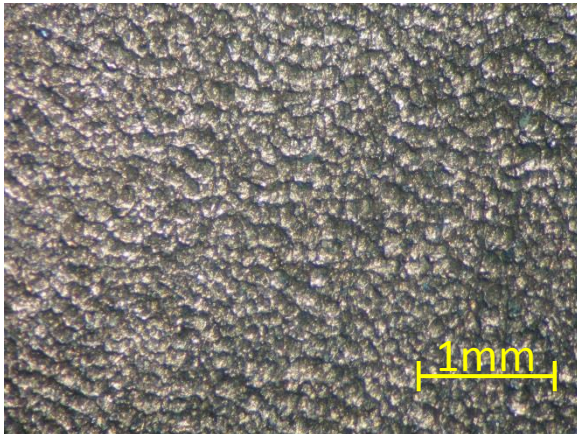
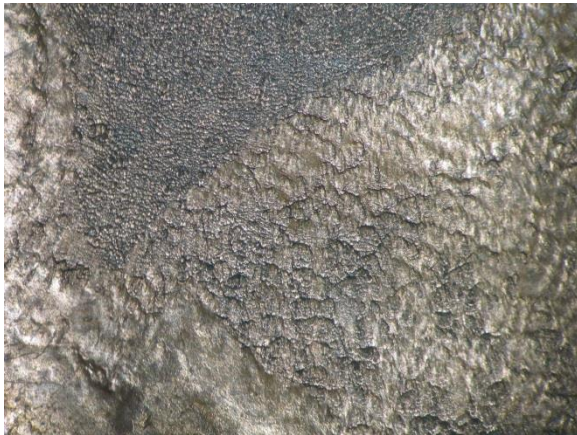
# Impact velocity

- Impact velocity vs Explosive/flyer mass ratio:  $V_p(R)$

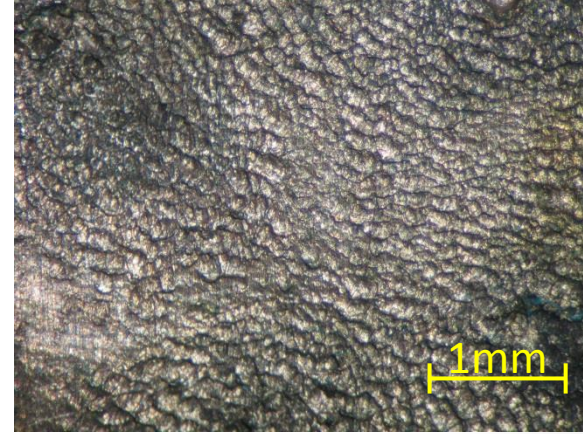
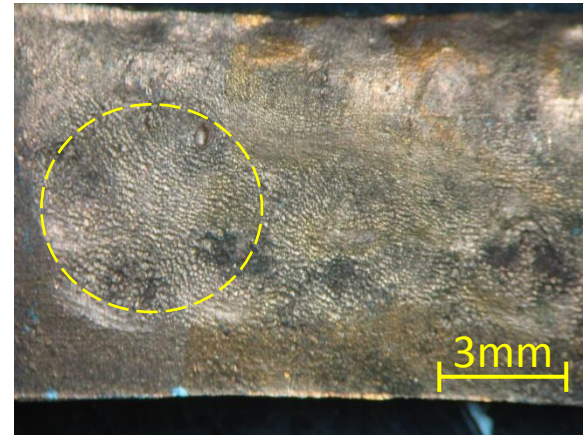


# Copper surface in contact with explosive- I

**EX + 15% HGMB**



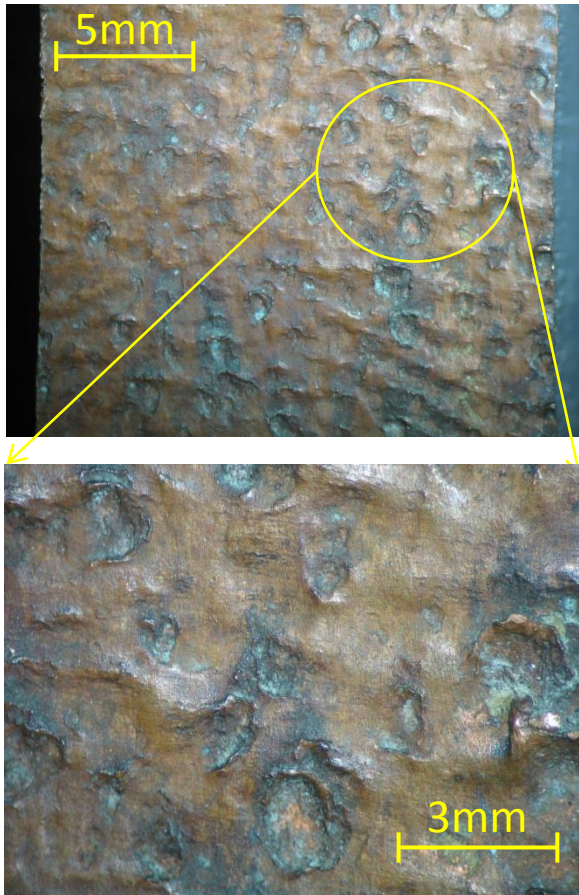
**EX + 1.2% EPS**



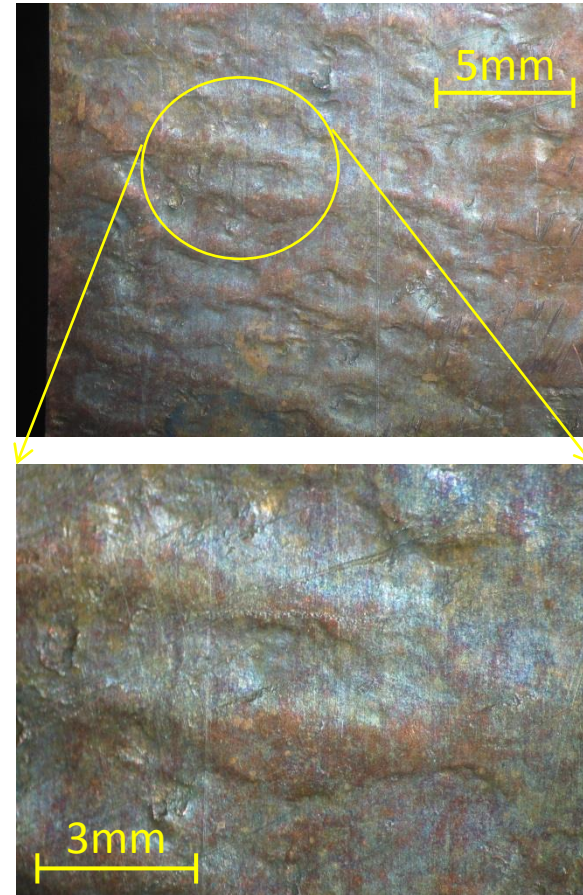


# Copper surface in contact with explosive- II

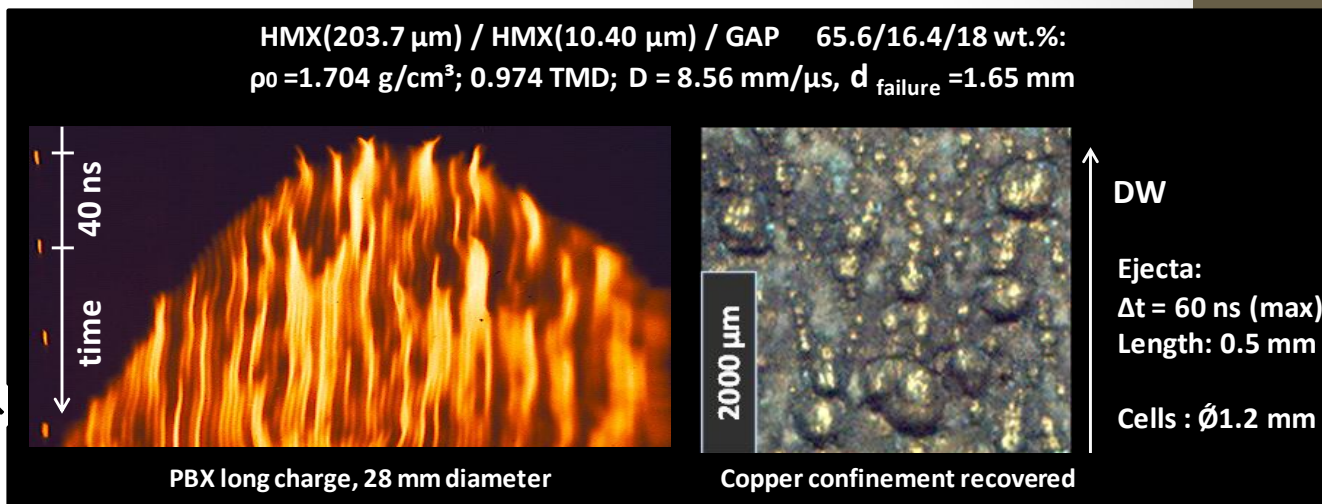
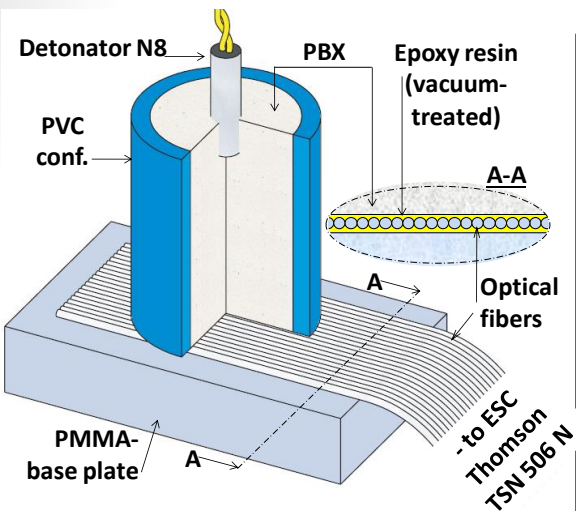
**ANFO + 20% EX**



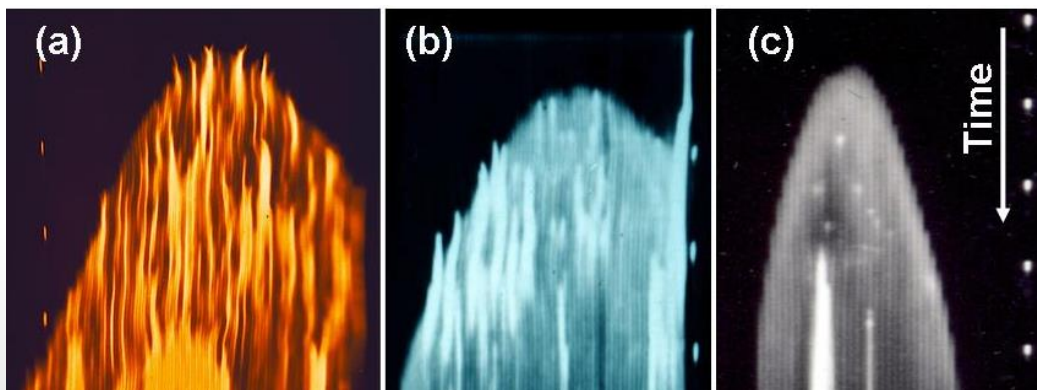
**ANFO**



# Effect of Ejecta-driven detonation cells on the boundary layer of copper confinement



- ➔ Spatially-resolved registration of the DRZ-localizations was performed with application of 96-channel optical analyzer MCOA-UC.
- ➔ Bright spots are corresponding to high-Temperature localizations (visible and near-IR radiation);
- ➔ Reaction localizations produce significant perturbations in the boundary layer of copper-confinement & PBX-driven liner (recovered copper-confinement is shown in the left image)

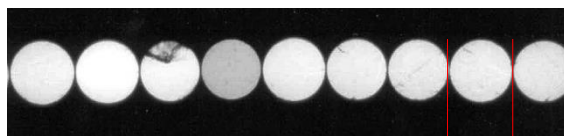
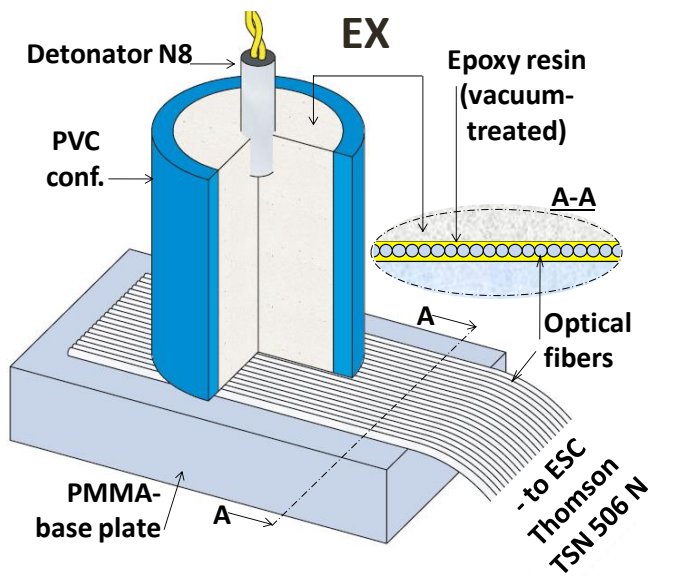


$\text{PBX}_{\text{st}}$  (a),  $\text{HMx}_L/\text{Water}$  (b) and  $\text{HMx}_F/\text{Water}$  (c). 40ns

Plaksin et al. 2001, 2003, 2005

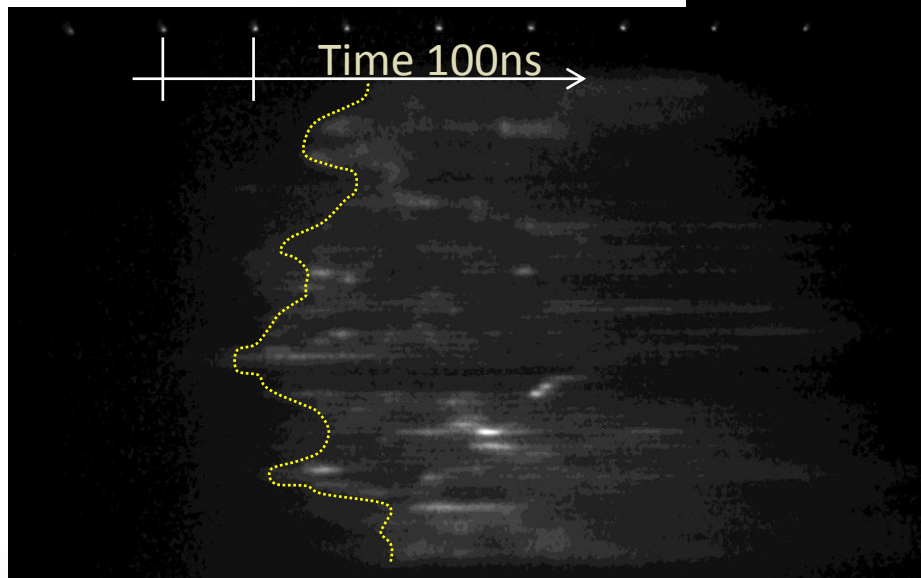
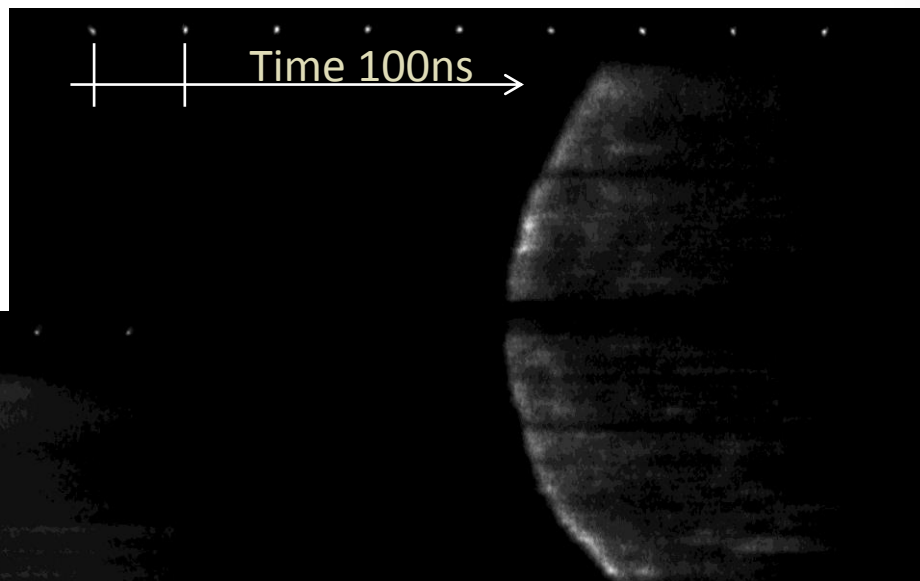


# Energetic Material: Detonation Front



250 μm

EX + 15% HGMB

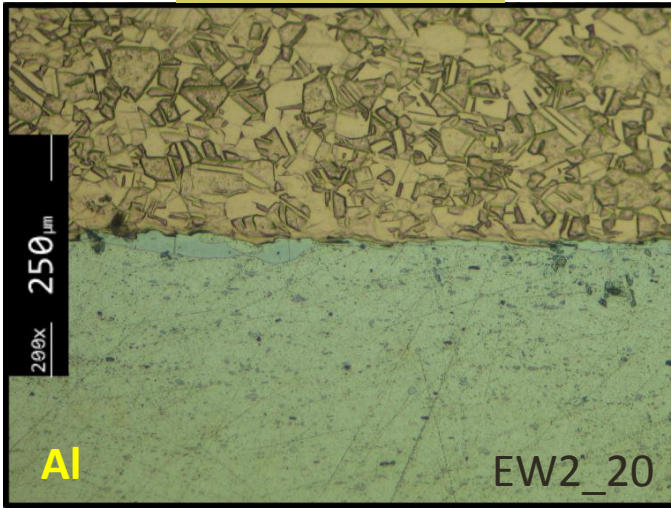


EX + 1.2% EPS

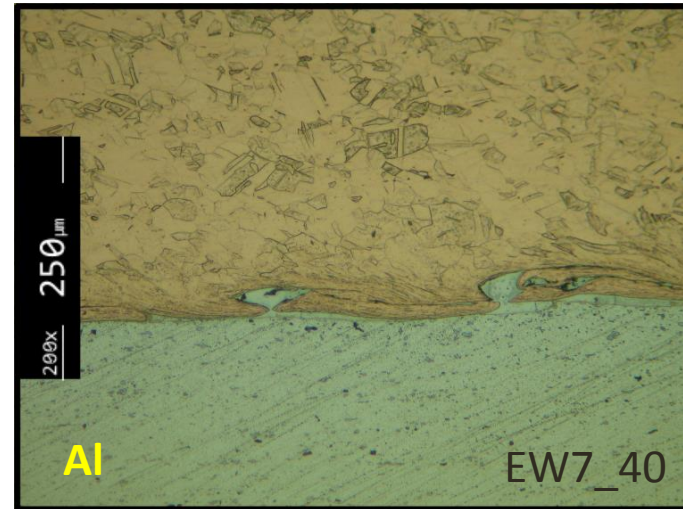
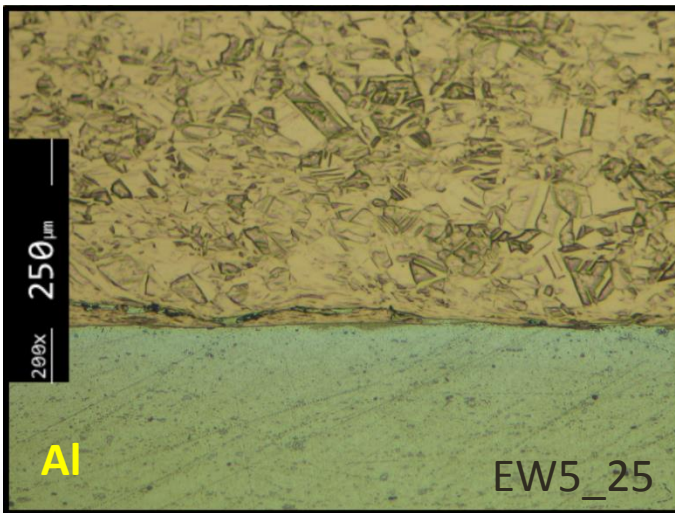
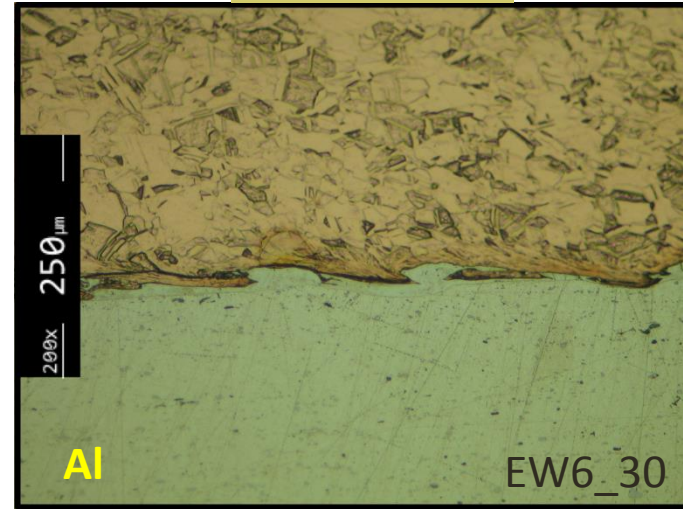


# Results: Interfacial waves

EX+15%HGMB

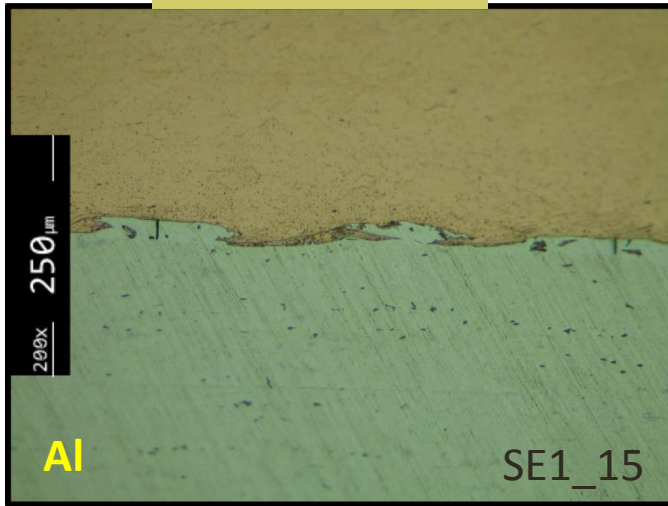


EX+1.2%EPS

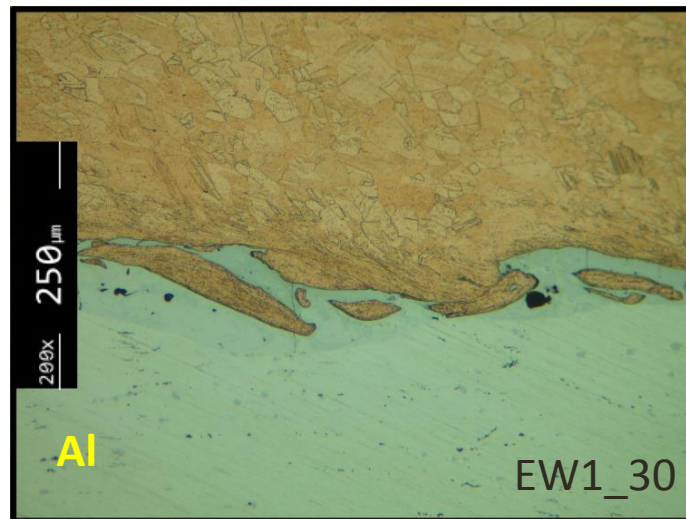
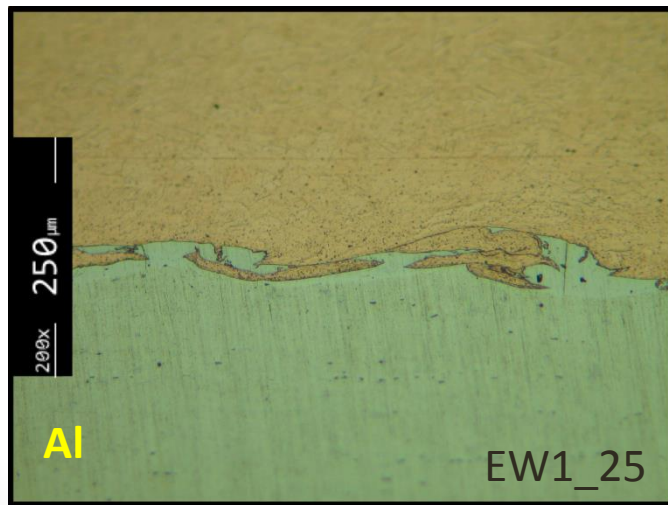
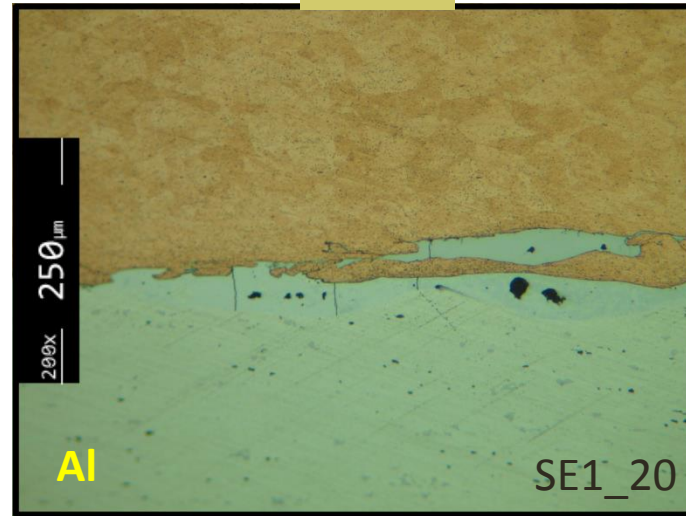


# Results: Interfacial waves

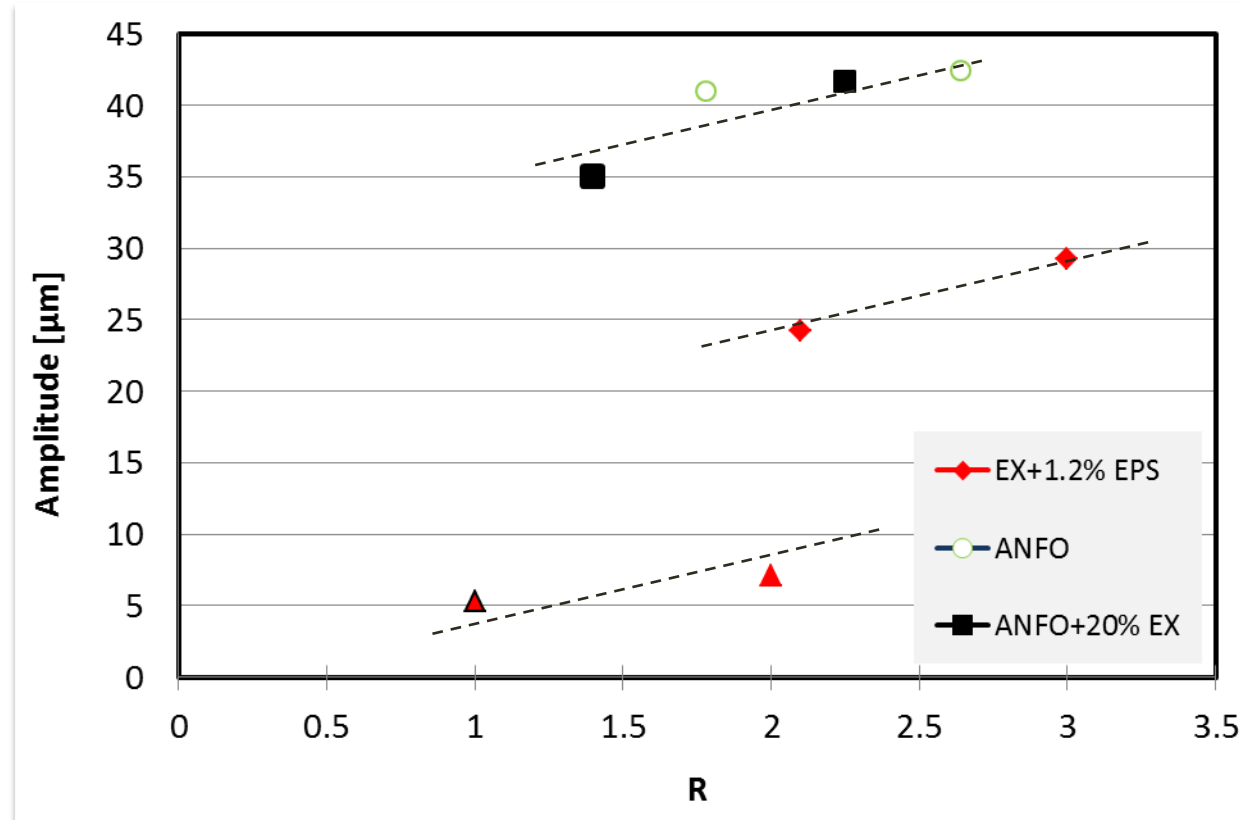
ANFO + 20%EX



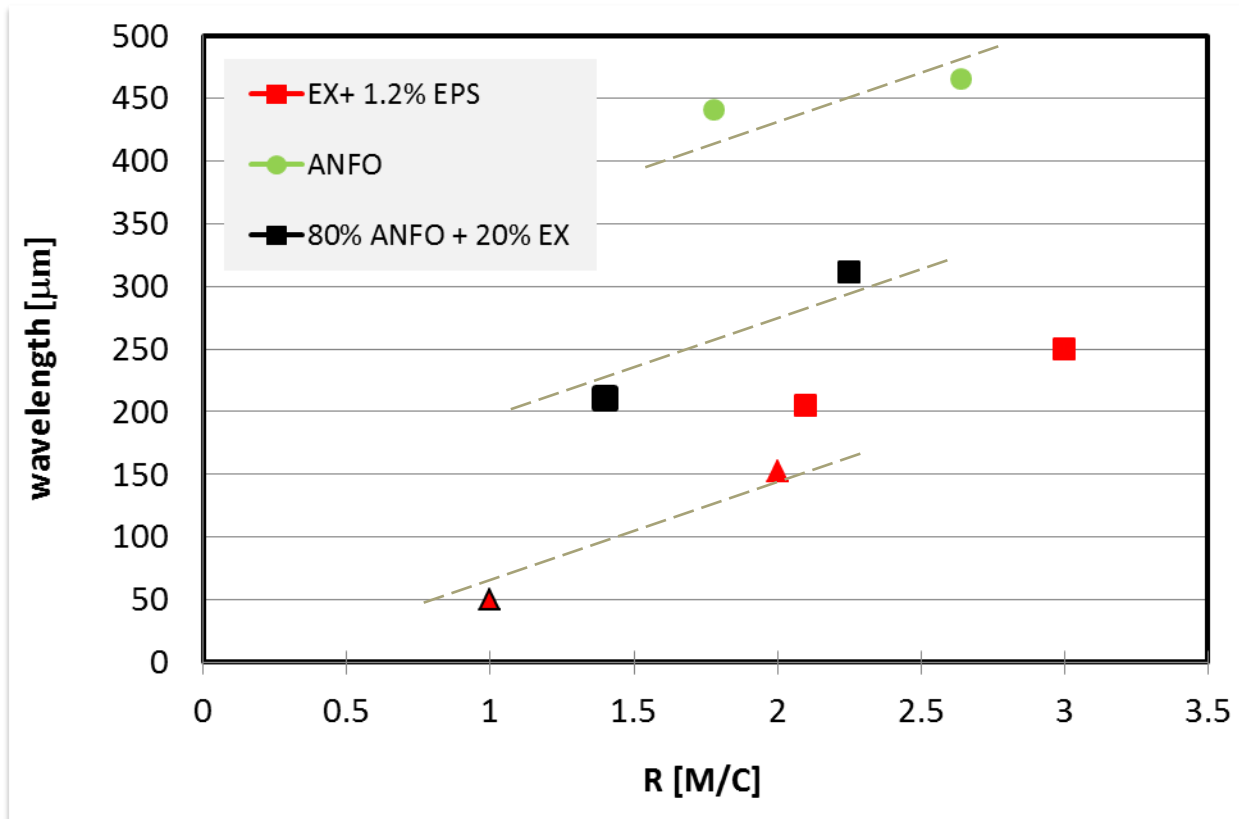
ANFO



# Wave amplitude vs R



# Wavelength vs R

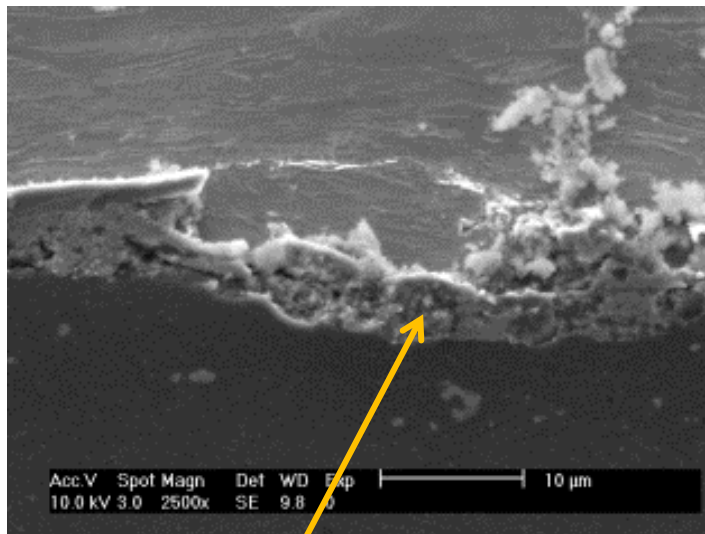


# Results: Intermetallics compounds

**SEM** and **EDS** analysis to interface zone have shown the formation of intermetallics compounds.

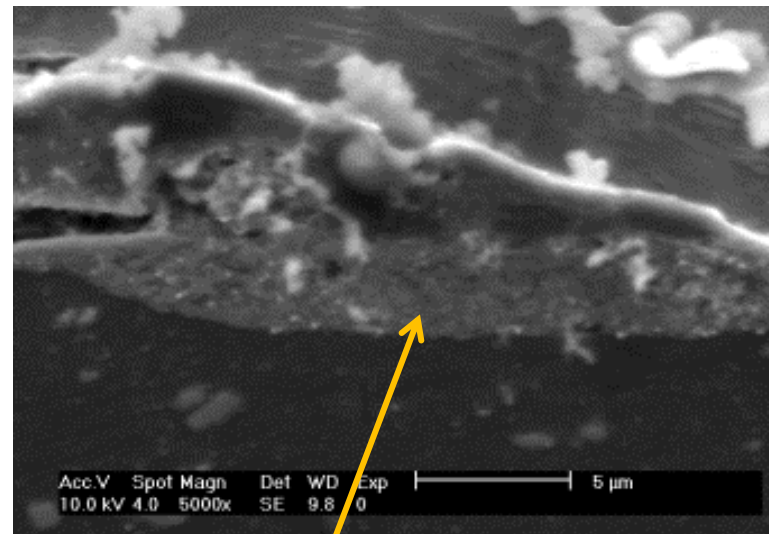
Thickness of intermetallic compounds band increases with increase of R

EX+15% HGMB (zone 1)



- Any known phase.

EX+15% HGMB (zone 2) EW2



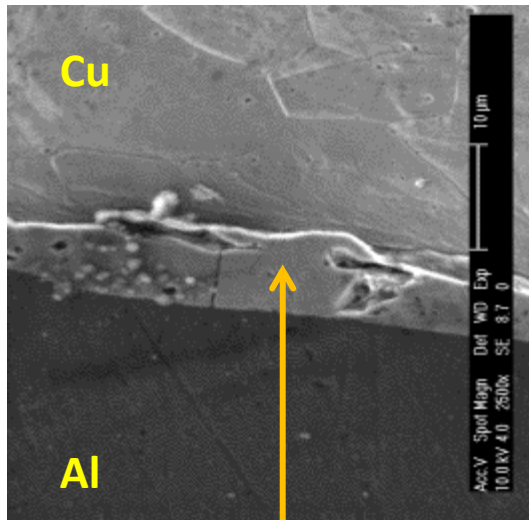
- Atomic composition close to  $\text{CuAl}_2$ , (Hang et. al., 2008)



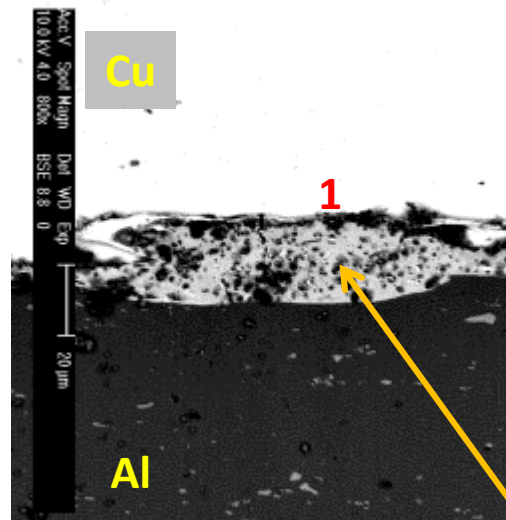


# Results: Intermetallics compounds

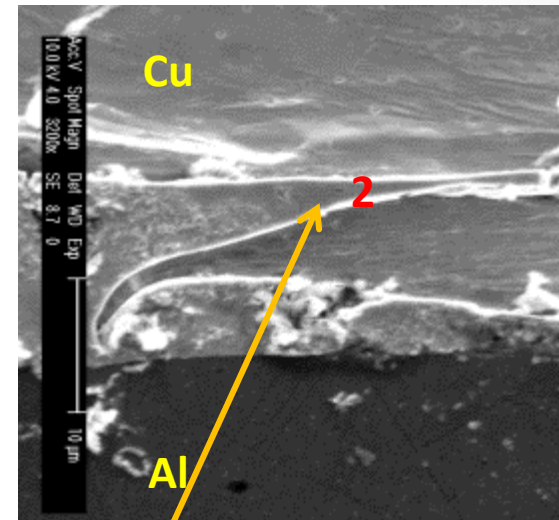
EW5- EX+15% HGMB



EW6- EX+1.2% EPS - 1



EW6- EX+1.2% EPS - 2



Intermetallic compound in EW5:



Intermetallic compound in EW6:

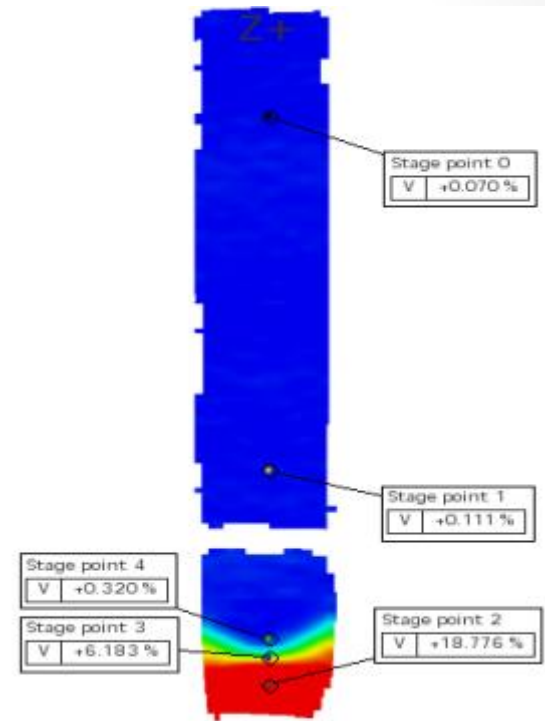
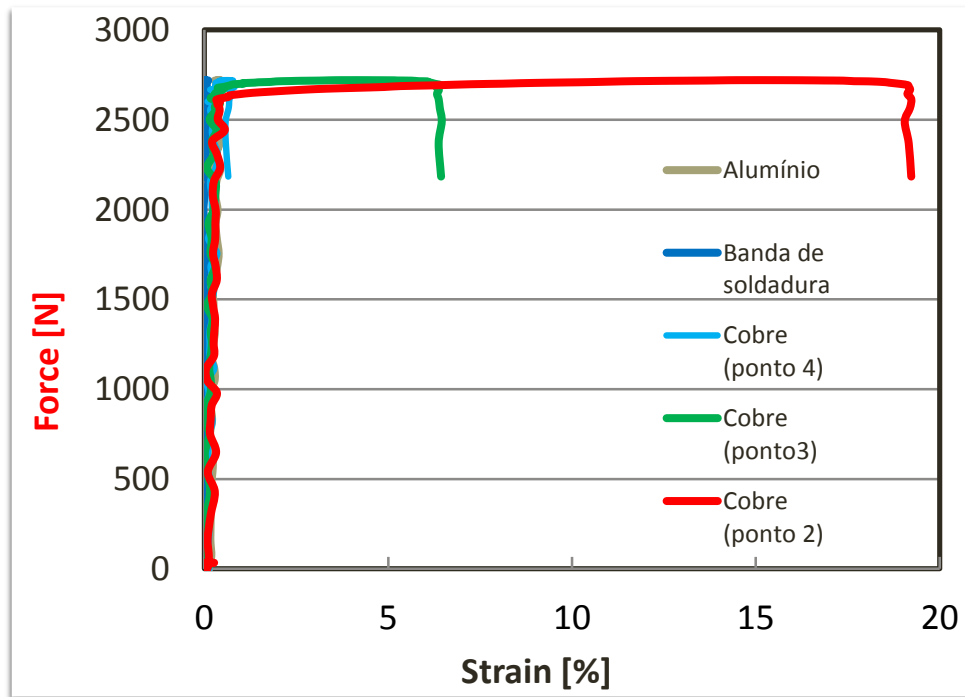
Zone 1 :  $\approx \text{CuAl}_2$ .

Zone 2 :  $\approx \text{CuAl}$



# Results: Tensile tests

Deformação EW2\_20\_3



Tensile Tests of the welds revealed that plastic deformation occurs in the Copper material for specimen prepared with EX+15%HGMB and with Ex+1.2% EPS.

The joint was able to transfer load, similar to an overlap weld.

# Conclusions

- The increase of R leads to the formation of bigger intermetallic zones with the formation of  $\text{CuAl}_2$  and  $\text{CuAl}$ .
- Tensile Strength of Al-Cu joint laps is higher than tensile strength of Cu.
- Fluctuations in detonation flow are a function of the explosive nature. Local fluctuations in detonation flow are transmitted to the metal surface, in contact with explosive, inducing on it a crater pattern that is function of the explosive nature.
- Beyond the parameters ( $V_p$ ,  $sod$ ,  $R$ ) that influence the wavy pattern, the local fluctuations in detonation flow play an important role on the characteristics of the interfacial waves.





# Thank you for your attention



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